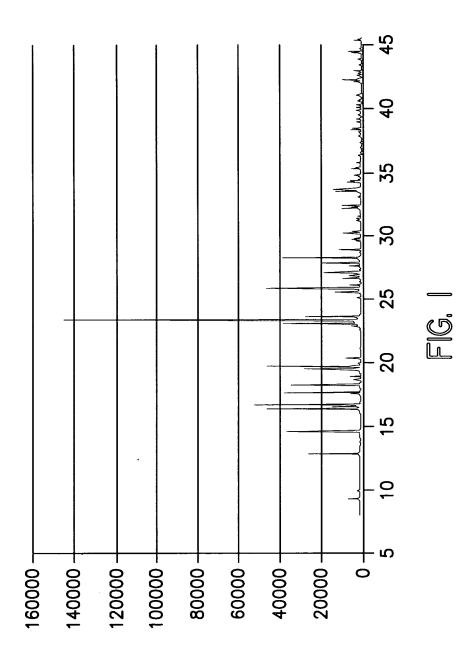
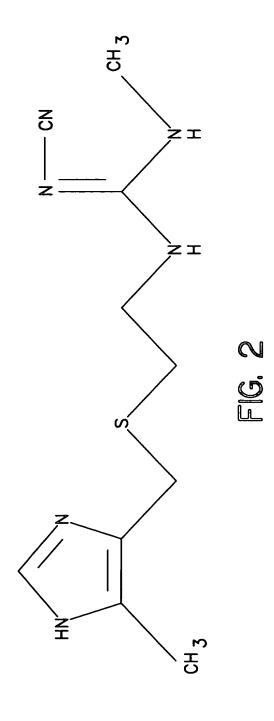
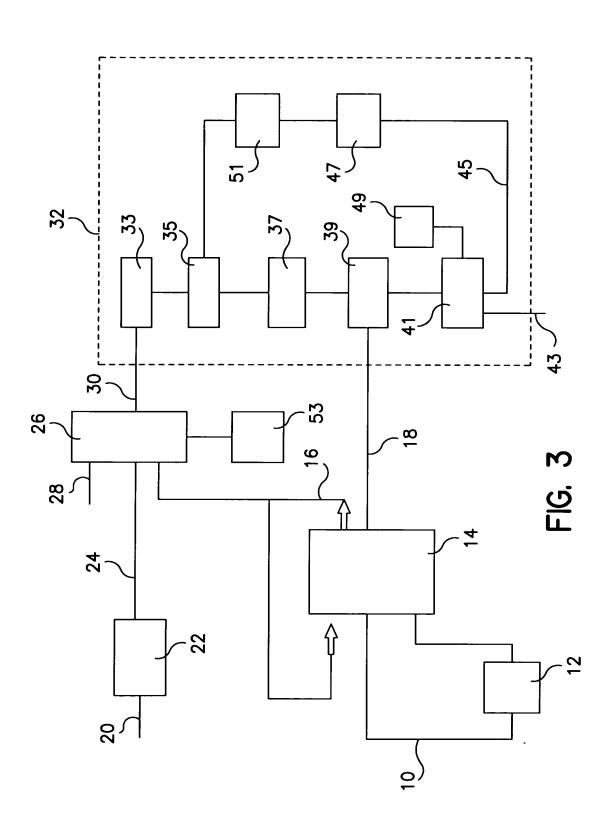
APPROVED	O.G. FIG.				
BY	CLASS SUBCLASS				
DRAFTSMAN					



APPROVED					
BY	CLASS	SUBCLASS			
DRAFTSMAN					



APPROVED	O.G. FIG.			
BY	CLASS SUBCLASS			
DRAFTSMAN				



APPROVED	O.G. FIG.				
BY	CLASS SUBCLASS				
DRAFTSMAN					

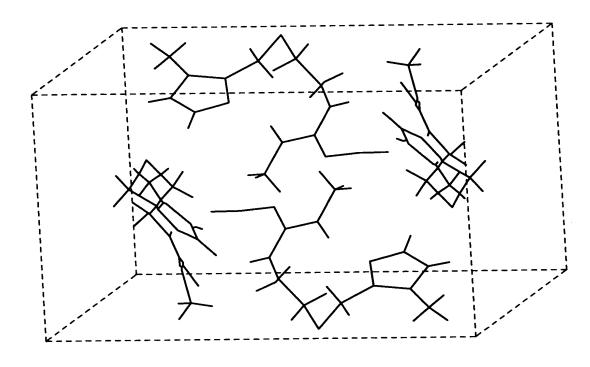


FIG. 4

APPROVED	O.G. FIG.				
ву	CLASS	SUBCLASS			
DRAFTSMAN					

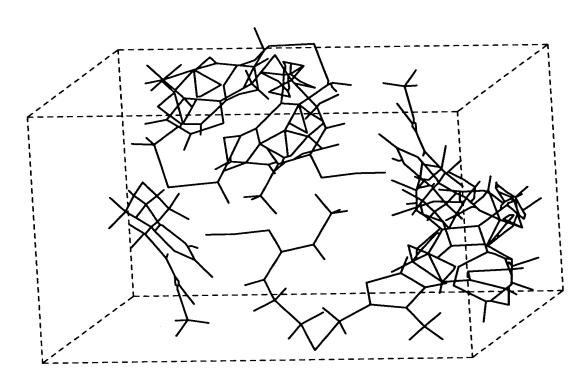


FIG. 5a

APPROVED	O.G. FIG.				
BY	CLASS SUBCLAS				
DRAFTSMAN					

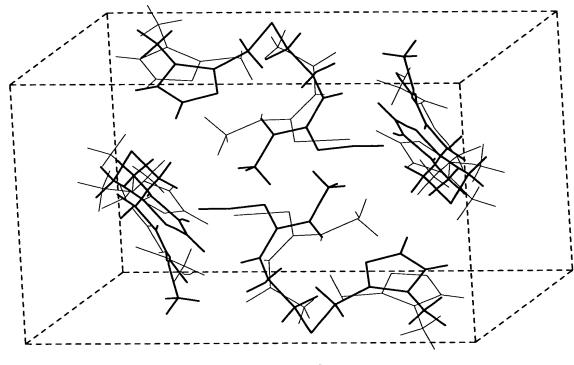


FIG. 5b

	/ED O.G. FIG.			
BY	CLASS SUBCLASS			
DRAFTSMAN				

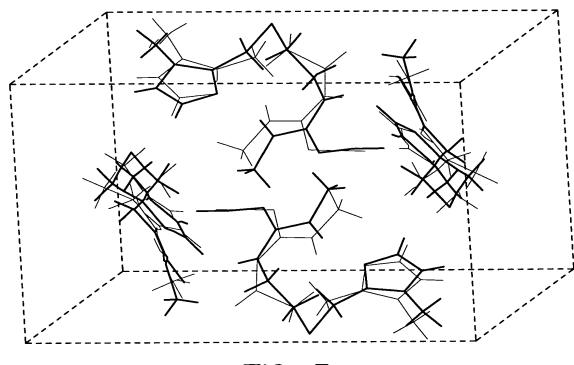


FIG. 5c

APPROVED	O.G. FIG.					
BY	CLASS SUBCLASS					
DRAFTSMAN						

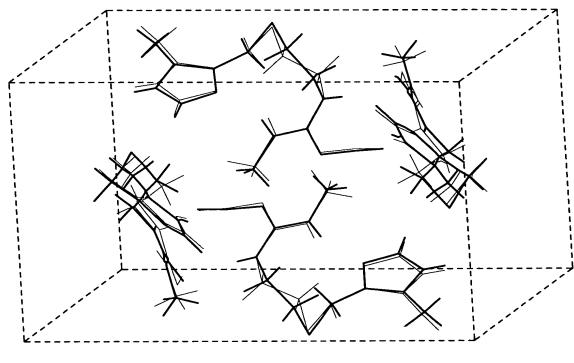
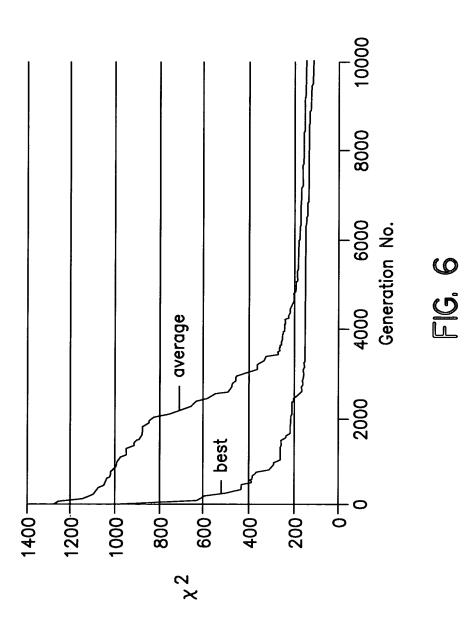
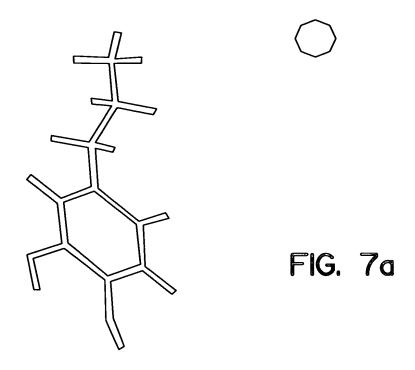


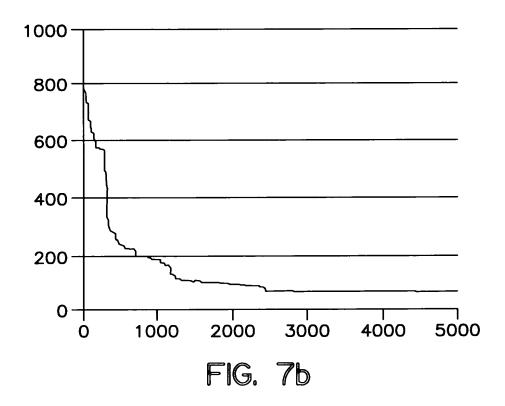
FIG. 5d

APPROVED	O.G. FIG.					
BY	CLASS SUBCLASS					
DRAFTSMAN						



APPROVED	O.G. FIG.			
BY	CLASS SUBCLASS			
DRAFTSMAN				





APPROVED					
BY	CLASS SUBCLASS				
DRAFTSMAN					

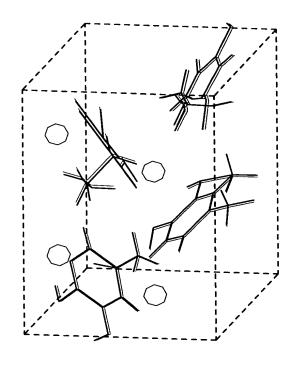
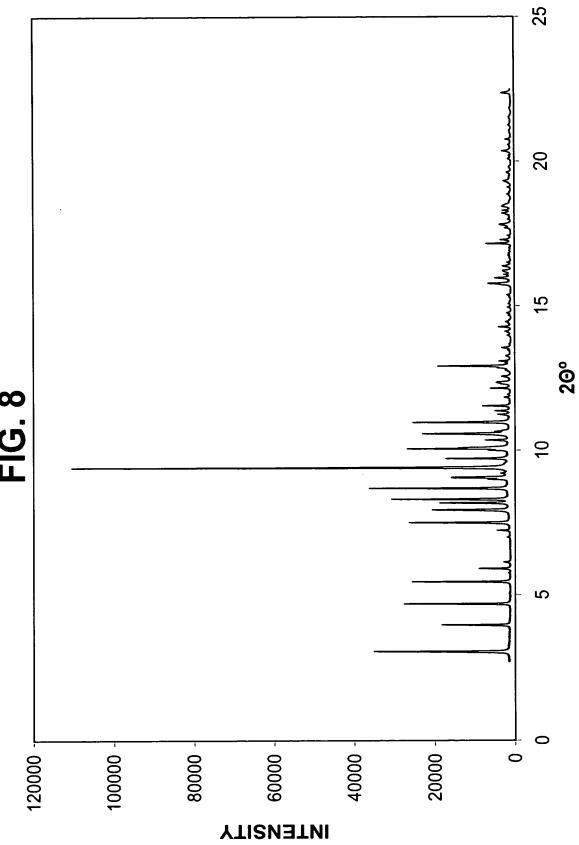


FIG. 7c

APPROVED O.G. FIG.
BY CLASS SUBCLASS
DRAFTSMAN



APPROVED O.G. FIG.

BY CLASS SUBCLASS

DRAFTSMAN

## FIG. 9

-	A	В	С	D	E	F	G	Н	I	J	K	L
1	1	0	0	10.047	0.1106	1	0	0	0	0	0	0
2	-1	1	0	3.637	0.0617	2	0	0	0	0	0	0
3	0	1	1	6.764	0.0874	3	0	0	0	0	0	0
4	0	2	0	0.321	0.0666	4	0	0	0	0	0	0
5	-1	1	1	8.983	0.1116	5	0	0	0	0	0	0
6	1	1	1	0.284	0.0432	6	0	0	0	0	0	0
7	-1	2	0	3.956	0.0916	7	0	0	0	0	0	0
8	2	0	0	2.070	0.1117	8	0	0	0	0	0	0
9	0	2	1	-0.025	0.0446	9	0	0	0	0	0	0
10	-2	1	0	0.005	0.0493	10	0	0	0	0	0	0
11	-1	2	1	0.375	0.0660	11	0	0	0	0	0	0
12	1	2	1	2.156	0.0959	12	0	0	0	0	0	0
13	-2	1	1	21.121	0.2266	13	0	0	0	0	0	0
14	0	0	2	10.592	0.4909	14	-55	34	0	0	0	0
15	2	1	1	9.634	0.6372	15	-88	0	0	0	0	0
16	-2	2	0	9.055	0.5427	16	0	Ó	0	0	0	0
17	-1	3	0	17.781	0.2205	17	0	0	0	0	0	0
18	<b>-1</b>	0	2	8.314	0.5049	18	-57	0	0	0	0	0
19	0	1	2	26.368	0.3353	19	0	0	0	0	0	0
20	0	3	1	0.385	0.0972	20	0	0	0	0	0	0
21	-1	1	2	2.992	0.2855	21	-59	0	0	0	0	0
22	1	0	2	23.776	0.2748	22	0	0	0	0	0	0
23	-2	2	1	23.776	0.2748	22	0	0	0	0	0	0
24	-1	3	1	5.447	0.1809	23	0	0	0	0	0	0
25	1	1	2	10.351	0.3342	24	-59	0	0	0	0	0
26	2	2	1	16.338	0.3506	25	o	0	0	0	0 .	0
27	1	3	1	0.341	0.1841	26	-69	0	0	0	0	0.
28	3	0	0	4.652	0.3947	27	0	0	0	0	0	0
29	0	2	2	137.393	0.6686	28	0	0	0	0	0	0
30	-3	1	0	1.685	0.1391	29	0	0	0	0	0	0
31	-2	0	2	0.293	0.3221	30	-28	0	0	0	0	0
32	1	2	2	21.709	0.3157	31	-23	0	0	0	0	0
33	-2	3	0	0.647	0.1616	32	0	0	0	0	0	0
34	-2	1	2	6.018	0.2122	33	0	0	0	0	0	0
35	1	2	2	34.450	0.4173	34	-39	0	0	0	0	0
36	-3	1	1	14.637	0.3554	35	-31	0	0	0	0	0
37	0	4	0	12.411	0.4668	36	0	0	0	0	0	0
38	2	0	2	17.335	0.5226	37	-53	0	0	0	0	0
39	-2	3	1	1.605	0.2200	38	0	0	0	0	0	0
40	-3	2	Ō	2.854	C.1700	39	0	0	0	0	0	0
41	-1	4	0	22.869	0.2070	40	0	0	0	0	0	0
42	3	1	1	22.869	0.2070	40	0	0	0	0	0	0
43	2	1	2	4.788	0.2129	41	-27	0	0	0	0	0
44	2	3	1	1.945	0.1824	42	0	0	0	0	0	0
45	0	4	1	-0.298	0.1358	43	0	0	0	0	0	0
46	-2	2	2	0.088	0.1723	44	0	0	0	0	0	0
47	0	3	2	44.292	0.5083	45	-48	0	0	0	0	0
48	3	2	1	3.714	0.3270	46	0	0	0	0	0	0
49	<del>  -1</del>	4	1	1.319	0.1982	47	-44	0	0	0	0	0
50	-1	3	2	4.787	0.2325	48	0	0	0	0	0	0
51	1	4	1	7.086	0.2216	49	0	0	0	0	0	0
52	3	2	1	-0.509	0.1419	50	e	0	0	0	0	0
,	, –	. –				1						

APPROVED	O.G. FIG.	
BY	CLASS	SUBCLASS
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